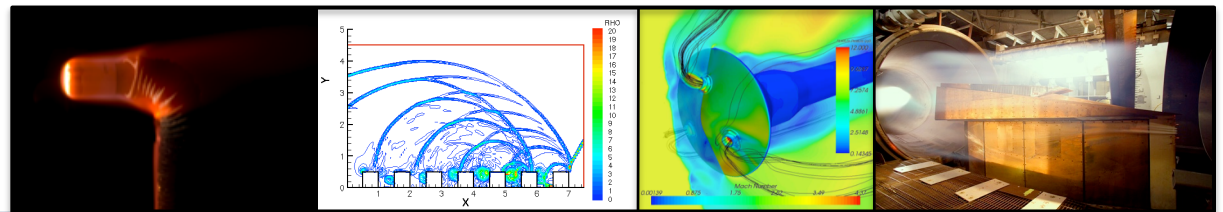




# Optimization and Fabrication Studies in the Development of Structurally Integrated Thermal Protection System Technology

**Mr. Craig Stephens, Element Lead**



# Outline

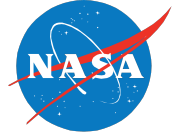
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- **Overview of near- and far-term structurally integrated thermal protection system (SITPS) efforts**
  - Process for vehicle level airframe analysis and design
  - Hypersonic vehicle acreage TPS options
    - Insulated, stand-off, SITPS characteristics
    - Comparison and implications of the various options
  - Background on the current SITPS efforts under HYP M&S
    - SITPS-0: Testing
    - SITPS-1: Design, manufacturing and test
    - SITPS-2: Design
    - SITPS Alternate Core: Development
  - Conclusions

# Acknowledgements

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# **Process for Vehicle Level Airframe Analysis and Design**

# Hypersonic Vehicle Airframe Analysis and Design Methodology

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- **Vehicle FEA model incorporating a representation of both the airframe substructure and acreage TPS are developed**
  - Vehicle acreage TPS is modeled (e.g. build an equivalent plate model) to produce effective stiffnesses for use in vehicle level model
  - **Nature of the TPS (insulated, stand-off, or SITPS) dictates the modeling of the load transfer from panel-to-panel (PtoP) and panel-to-airframe substructure (PtoAS)**
- **Vehicle global loads (aerodynamic, aerothermal, and aerostructural) are applied to vehicle FEA model to produce nodal  $\{U\}$ ,  $\{Q\}$ , and temperature vectors for entire vehicle**
  - Areas of high deformations, high temperatures, high thermal gradients are candidate areas for submodel investigation

# Hypersonic Vehicle Airframe Analysis and Design Methodology

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- **For a specific critical region, submodels are constructed and subjected to appropriate temperatures, loads and displacement boundary conditions for these regions**
  - Detailed 3D FEA submodels of the specific elements (corrugated core, sandwich structures, etc.) are used
  - Stresses within individual elements are determined and Margin-of-Safety (MOS) values are calculated
  - Negative MOS and / or high MOS require changes to the acreage design elements
- **When submodel designs are obtained with all positive MOS, updated [A], [B] and [D] matrices of acreage regions are used in full vehicle model to produce new {U}, {Q}, and temperature vectors for entire vehicle**
  - Submodels are re-analyzed with new {U} and {Q} to check that all MOS are still positive



# **Hypersonic Vehicle Acreage TPS Options**

# Vehicle Trajectory Impact on TPS Needs

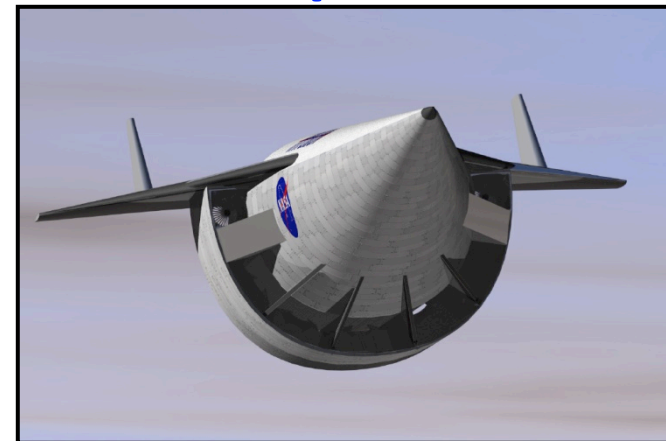


## Re-Entry Vehicles



- Higher peak heating rates over shorter time periods
  - Yields higher surface temperatures
- Lower integrated heat loads
  - Vehicle thermal management systems typically not required
  - Vehicle cooling provided by ground support equipment soon after landing
- Mechanical / thermal loads out-of-phase

## Trans-Atmospheric Vehicles



- Lower peak heating rates over longer time periods
  - Yields lower surface temperatures
- Higher integrated heat loads
  - Vehicle thermal management a critical consideration in vehicle design and operation
- Mechanical / thermal loads in-phase



# TPS Options – Vehicle Acreage\*



- **Insulated Structure**

- Insulators (tiles or blankets) are attached directly to the cold structure to form the outer mold line (OML) of the vehicle
  - Insulators are for thermal performance and transfer some aerodynamic (pressure only) loads to the inner structure, but no thermal loads
  - Inertial loads are carried by the internal vehicle structure
  - Example: Space Shuttle acreage TPS



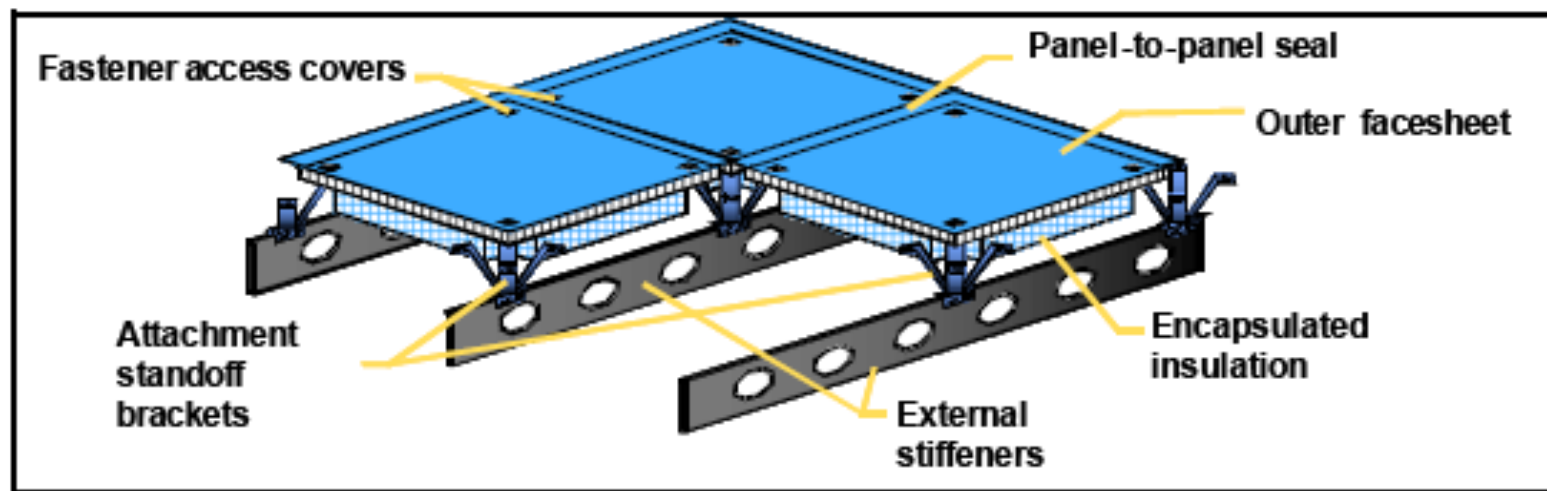
\*Glass, David E., "Ceramic Matrix Composite (CMC) Thermal Protection Systems (TPS) and Hot Structures for Hypersonic Vehicles," AIAA-2008-2682, 2008.

# TPS Options – Vehicle Acreage\*



- **Stand-off TPS**

- TPS system is “isolated” so aerodynamic (pressure only) loads and not thermal loads can be directly transferred to the internal vehicle structure
  - Typically consist of more parts but can form an OML of a different contour than the internal vehicle structure
  - Insulation is required on the panel inner mold line (IML)
  - Example: X-33



\*Glass, David E., “Ceramic Matrix Composite (CMC) Thermal Protection Systems (TPS) and Hot Structures for Hypersonic Vehicles,” AIAA-2008-2682, 2008.

# Vehicle Trajectory and TPS



- **Vehicle Design Level**

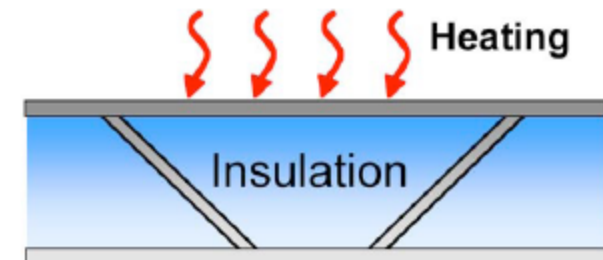
- Internal systems need to be thermally protected in a volumetric efficient manner
  - Vehicle design options
    - **Application of external insulation (i.e. insulated structure)**
    - **Less external insulation but additional internal insulation and / or thermal management systems**
- Design option becomes insulating at the OML only or insulating at both the OML and at the individual internal systems?
- Is there another option? Can you develop a method for insulation application that is both structurally and volumetrically efficient?
  - **This goal is the driver for NASA's SITPS development**
    - **The development of an advanced TPS that is both structurally and volumetrically efficient using high-temperature ceramic matrix composite and light-weight insulation materials**

# TPS Options – Vehicle Acreage\*



- **Structurally Integrated Thermal Protection Systems**

- “A TPS that has both an integrated (mechanical and thermal) load carrying capability and an ability to share mechanical loads with adjacent TPS structures”
  - SITPS is designed to carry both aerodynamic (pressure & shear) and inertial loads
  - Outer and inner walls carry airframe loads, with outer wall operating hot and the inner wall insulated
  - For SITPS panels to be structurally efficient, mechanical loads (i.e. bending moments, shear, and torques) must occur across adjacent panels
    - If this does not occur, all panels behave as “simply supported,” thus behaving like a stand-off TPS
  - Potential Benefits of SITPS
    - Lower weight TPS, higher structural efficiency
    - Larger panel sizes possible, fewer seals, reduced gaps, and lower parts count
    - More durable TPS, lower maintenance
  - SITPS Design Options
    - Sandwich (e.g. honeycomb, foam filled, etc.)
    - Hat-stiffened
    - Rib-stiffened shell
  - Example: None (low TRL technology)

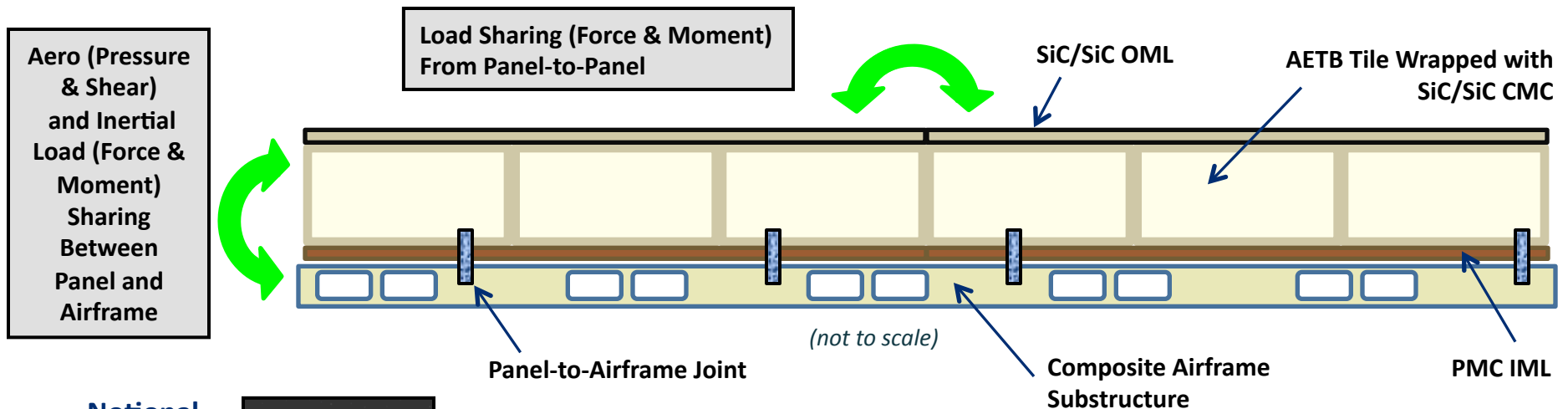
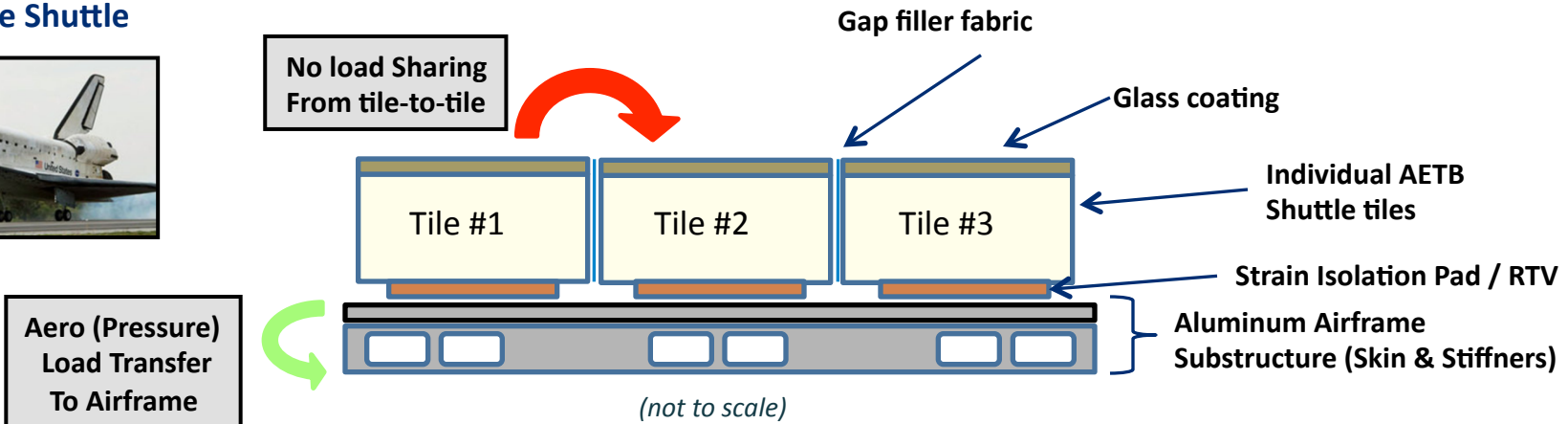


\*Glass, David E., “Ceramic Matrix Composite (CMC) Thermal Protection Systems (TPS) and Hot Structures for Hypersonic Vehicles,” AIAA-2008-2682, 2008.

# TPS Options – Vehicle Acreage Comparison



## Space Shuttle



## Notional Space Operations Vehicle



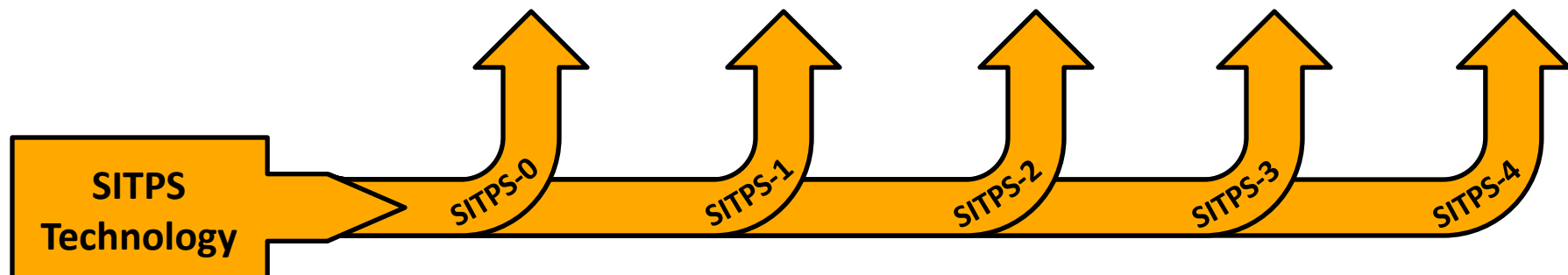
# SITPS Roadmap



- **ARMD Hypersonics Materials & Structures (M&S) Approach**

- Incrementally develop the required SITPS technology
- Continually integrate and test SITPS technology as it becomes available
- Document technology for future efforts

FY09				FY10				FY11				FY12				FY13			
Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4





# **HYP M&S SITPS Development**

## **Effort: SITPS-0**

# SITPS-0 Overview

## Manufacturing Demonstration Article



- **Goal**

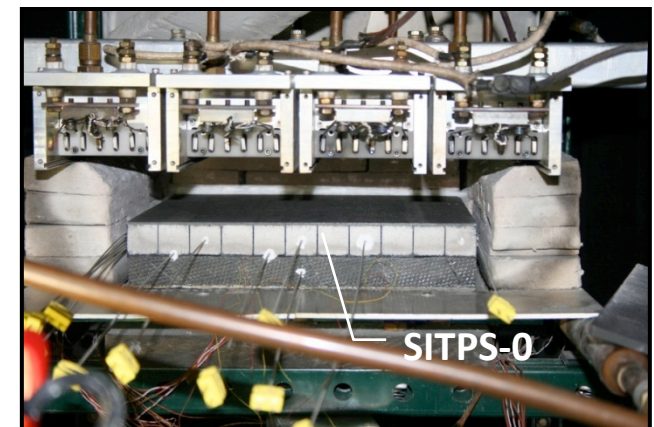
- Develop manufacturing capabilities (ATK-COIC)

- **SITPS-0 Details**

- Panel has no detectable defects
- 11.5 in. x 11.5 in. x 2.2 in. thick (approx.)
- Insulation core – AETB 16
- OML: S200H PIP SiC/SiC
- IML: M55J/954-3 Cyanate Ester
- Weight  $\sim 5.8 \text{ lb}_m/\text{ft}^2$

- **Panel is currently at NASA LaRC for thermal characterization testing**

- Steady-state measurements of “through-thickness” effective thermal conductivity ( $K_{\text{eff}}$ )
  - OML CMC side: isothermal conditions from 250°F to 2000°F
  - IML CE side: mounted to a water cooled plate
  - Pressure varied from 0.001 Torr to 760 Torr ( $10^{-6}$  to 1 atm)
- Transient measurements
  - Simulated re-entry pressure and surface temperature profiles
  - Used to validate (1) the  $K_{\text{eff}}$  data collected and (2) validate the thermal model developed for SITPS-0



**SITPS-0 in the LaRC  
Steady-State Thermal Test  
Apparatus**





# **HYP M&S SITPS Development**

## **Effort: SITPS-1**

# SITPS-1 Overview



- **Goal**

- Scale-up the SITPS-0 manufacturing capability
- Fabricate a panel for structural testing
  - Generate data to validate a model of the SITPS-1 concept

- **Process**

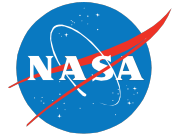
- Optimize the SITPS-0 Design
  - Reduce the panel area weight – goal is approximately 3 lb<sub>m</sub>/ft<sup>2</sup>
  - Reduce the disparities between failure loads between the OML and IML materials
- Address manufacturing issues with scaling up the optimized design to larger panel areas
- Develop a database of SITPS material strength and thermal performance

- **Results – SITPS-1 Panel Design Based on Optimization of SITPS-0**

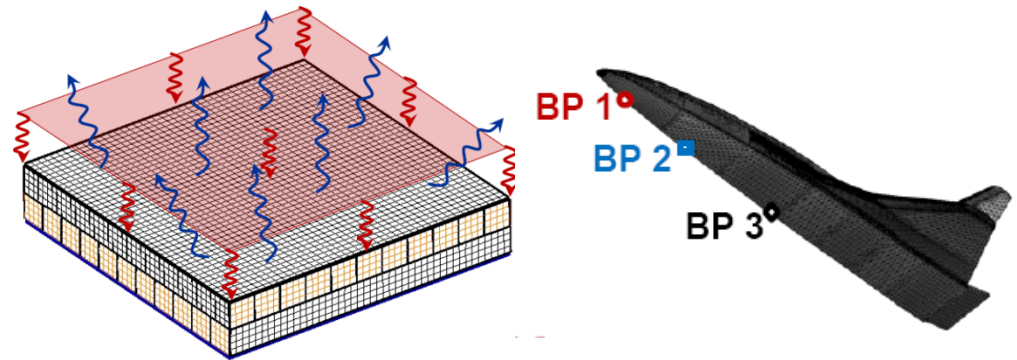
- Thermal analysis of the SITPS-0 performance for NASA HRRLS re-entry trajectory
  - Switched from AETB-16 to AETB-8 to help reduce area weight
  - Modified the IML temperature allowables from 400°F to 600°F
  - Modified AETB “bar” sizes to reduce area weight
- Structural analysis of the OML and IML to modify the ply layups to reduce the disparities between failure loads

# SITPS-0 Modeling\*

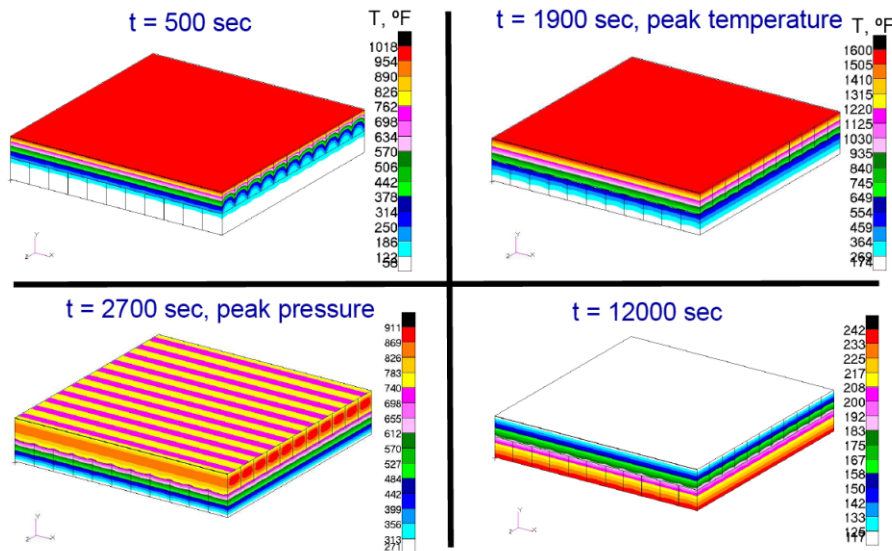
## Original Thermal Analysis



- Original SITPS-0 configuration
- Boundary Conditions
  - Uniform heat flux corresponding to a particular body point
  - Radiation to space
  - Insulated sides and bottom
- Material Temperature Limit Criteria
  - PMC and bondline  $\leq 400^{\circ}\text{F}$



- BP-2 maximum outer surface temperature  $\sim 1590^{\circ}\text{F}$



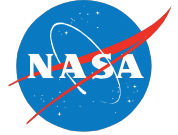
### Concluding Remarks

- The SITPS concept was sized for HRRLS upper stage re-entry heating, resulting in overall insulation thickness of  $\sim 3.7$ , 3.25, and 3 inches at 10, 25, and 50% of vehicle length (respectively)
- Thermal-stress analysis of the 3-inch thick panel indicates that the concept is viable at the fabricated panel scale

\* Bey, K., Butcher, K., and Easler, T., "Fabrication and Thermal Analysis of a Structurally-Integrated Thermal Protection System Concept," 33<sup>rd</sup> Annual Conference on Composites, Materials, and Structures, Cocoa Beach, FL, Jan. 26-29, 2009.

# SITPS-1 Optimization

## Thermal / Structural Analysis



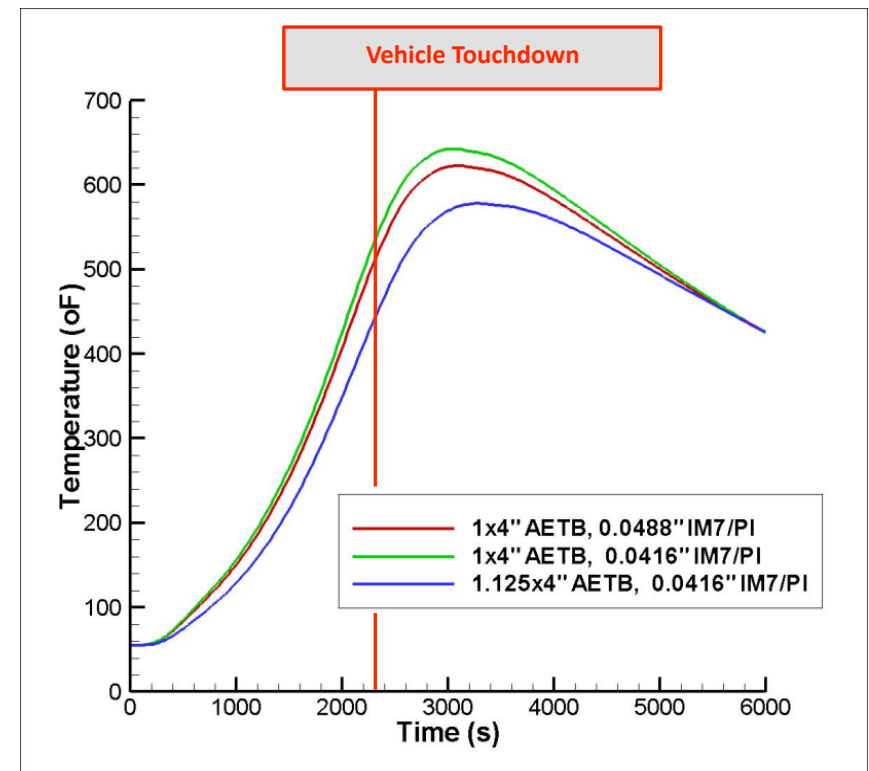
- **SITPS analysis changes**

- Switched from AETB-16 to AETB-8 to help reduce area weight
- Modified the IML temperature allowables from 400°F to 600°F
- Modified AETB “bar” sizes to reduce area weight
- Laminate analysis resulted in tailoring the OML and IML ply layups to reduce the disparities between failure loads

- **“Optimized” SITPS-1 Design**

- 4 plies of S200H as top facesheet
- 2 layers (thicker and wider) of AETB-8 core / insulation (alternating directions)
- 4 plies of T650-35/PI for the bottom facesheet

- **Area weight estimate = 3.1 lb<sub>m</sub>/ft<sup>2</sup>**

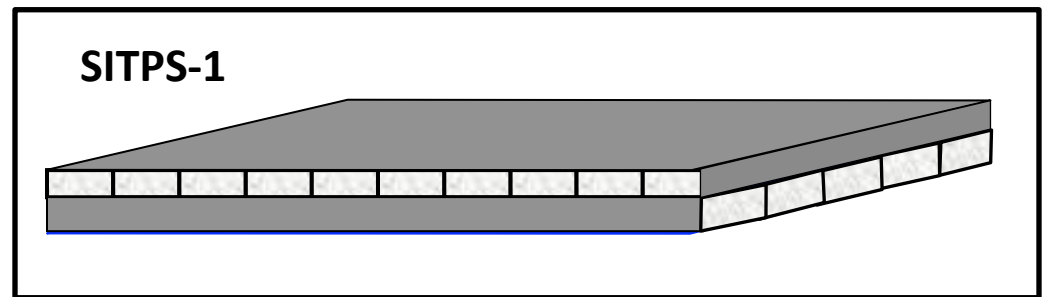


# SITPS-1 Status



- **ATK-COIC to manufacture larger panel for structural testing**

- 20 in. wide x 36 in. long x ~ 2.15 in. thick
- Insulation core – AETB 8
- OML: S200H PIP SiC/SiC
- IML: T650-35 Woven Polyimide

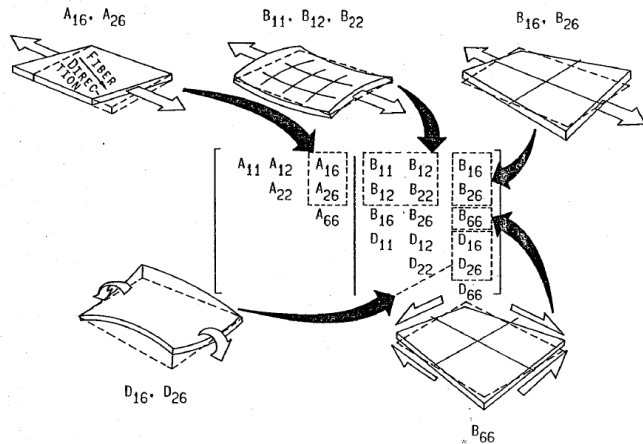
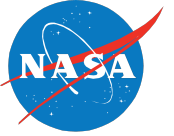


- **SITPS-1 panel fabrication initiated**

- Numerous panel fabrication issues have been addressed by the team
  - Estimate panel fabricated January 2010
- SITPS-1 to be structurally tested by September 2010
  - Currently working the design details of the structural tests
- Material database for the SITPS-1 components to be completed September 2010
  - Materials will be available November 2009
  - Thermal / structural testing to be completed by September 2009 and will be posted on the HYP M&S CMC Wiki site

# SITPS-1 Testing

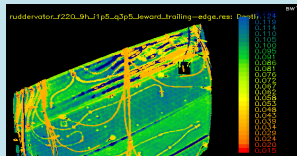
## Acquisition of Compliance Coefficient Information



- Coupling Phenomena in the SITPS-1 design
  - In-plane normal loads produce in-plane shear and bending and twisting curvatures
  - Bending loads produce in-plane distortions as well as bending & twisting curvatures

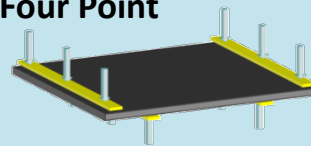
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Transient IR



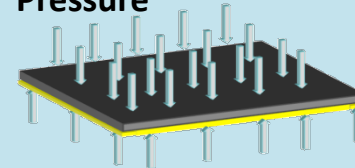
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Four Point



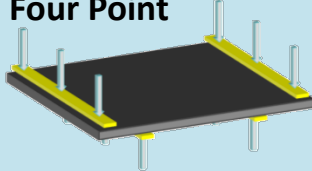
3

Pressure



4

Four Point



5

Tension



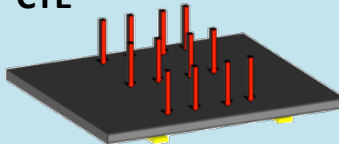
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Panel Shear



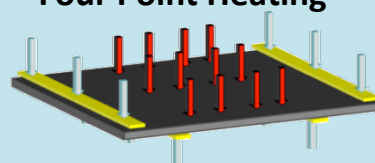
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CTE



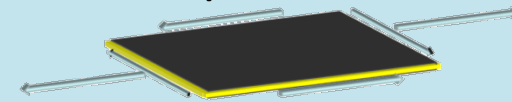
8

Four Point Heating



9

Tension / Shear



# SITPS Structural Test Plans



## Current Effort

Single-Panel Characterization Tests  
(Near-Term Goal)



Measured A, B, D  
compliance coefficients

M&S Vehicle  
Level Analysis

MDAO Analysis  
Using SITPS

## Future Effort

Multi-Panel Performance Tests  
(Long-Term Goal)

M&S development of generic PtoP  
and PtoAS attachment option(s)

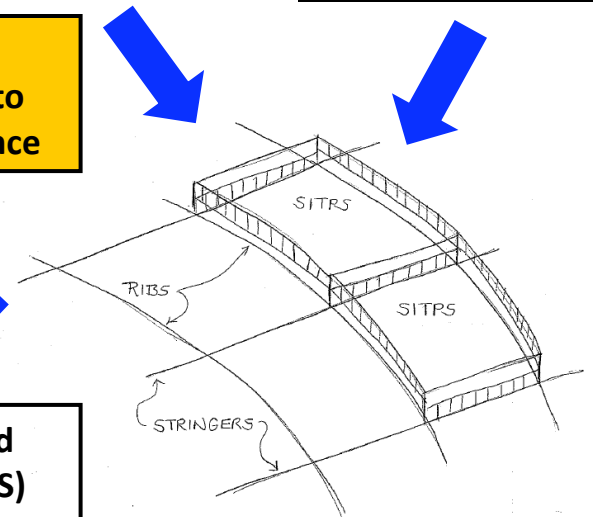
MDAO provides  
"vision vehicle"  
loads

M&S development of  
structural test methods to  
evaluate panel performance

- Quantified effective load transfer (PtoP and PtoAS)
- SITPS overall performance

Improved M&S Vehicle  
Level Analysis

Improved MDAO  
Analysis Using SITPS





# **HYP M&S SITPS Development**

## **Effort: SITPS-2**



# SITPS-2 Overview



- **Goal**

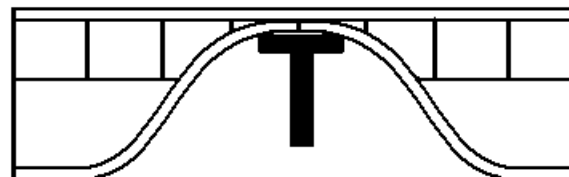
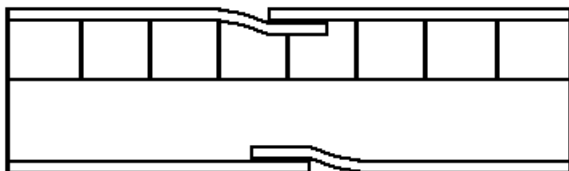
- SITPS-2A: Initiate the development of panel closeouts and panel-to-panel joints
- SITPS-2B: Develop manufacturing capability for curved SITPS panels

- **Process**

- SITPS-2A
  - Formulate panel-to-panel joint concepts that allow load and moment transfer between panels
  - Structurally test three sub-elements of potential joint designs
  - Down select to the most promising joint design for a larger panel development and testing
- SITPS-2B
  - Address manufacturing issues associated with the fabrication of a large-scale SITPS panel with single-direction curvature

- **Results – SITPS-2**

- Planning for SITPS-2A and SITPS-2B to begin in Oct 2009
  - Initiate the design discussion focusing on the development of SITPS-2A panel-to-panel attachment designs for

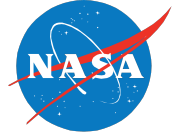




# **HYP M&S SITPS Development**

## **Effort: SITPS Alternate Cores**

# SITPS Alternate Core Overview



- **Goal**

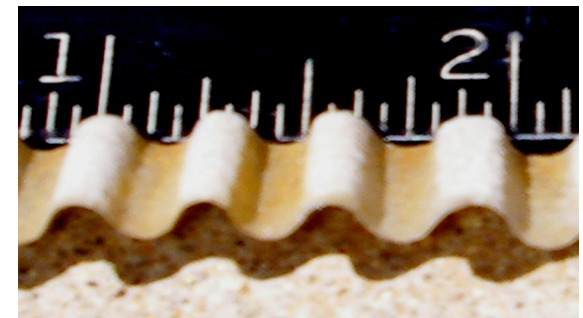
- Development of high-temperature core technology (i.e. honeycomb) for use with alternate SITPS designs

- **Process**

- Identify core materials and evaluate the materials for potential honeycomb fabrication
- Thermal / structural evaluation testing of candidate honeycomb sub-elements
- Conduct analytical study to examine the different core geometries (i.e. wall thickness, shape, height, etc.) and its effect on core thermal / structural properties
  - Goal is to define the best core geometry for SITPS applications
- Assess what material, core geometries, etc. that lend themselves to be scaled up to larger panels and ultimately vehicle use

- **Results – SITPS Alternate Cores**

- Current NRA has been re-directed to focus on SITPS requirements



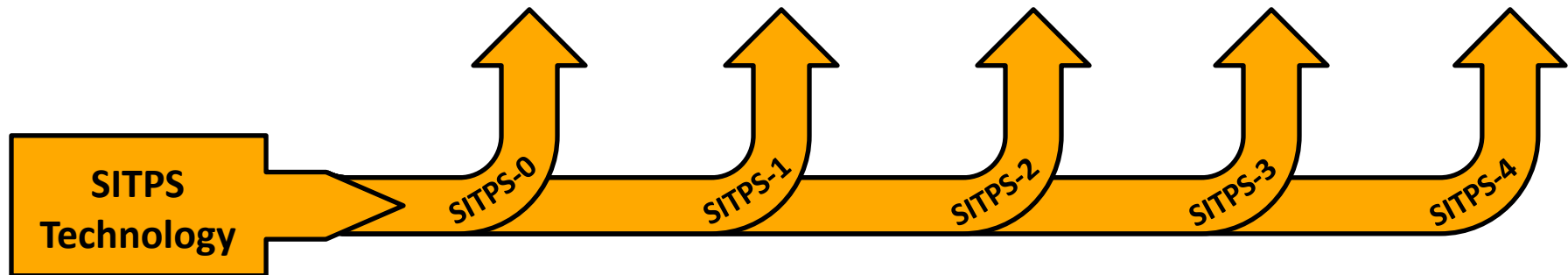


# Conclusions

# Conclusions



FY09				FY10				FY11				FY12				FY13			
Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4



- **NASA HYP M&S is pursuing the development of SITPS**

- Working with HYP MDAO to formulate methodology to incorporate SITPS into hypersonic vehicle design trades
- SITPS-0 to SITPS-1 (FY10)
  - Manufacturing development and weight reduction (5.8 to 3.1 lb<sub>m</sub>/ft<sup>2</sup>)
  - Structural testing to mature SITPS model
- SITPS-2 (FY11)
  - Focus on panel closeout, panel-to-panel load transfer, and panel curvature
- Extend fabrication technology to include alternate cores and insulations (FY12)